

# Design, Fabrication, and Measurement of Two Silicon-Based Ultraviolet and Blue-Extended Photodiodes

Changping CHEN<sup>1,2,3</sup>, Han WANG<sup>1,2</sup>, Zhenyu JIANG<sup>1,2</sup>,  
Xiangliang JIN<sup>1,2\*</sup>, and Jun LUO<sup>4</sup>

<sup>1</sup>Faculty of Materials, Optoelectronics and Physics, Xiangtan University, Xiangtan, 411105, China

<sup>2</sup>Hunan Engineering Laboratory for Microelectronics, Optoelectronics and System on A Chip, Xiangtan, 411105, China

<sup>3</sup>The forty-eighth Research Institute of China Electronics Technology Group Corporation, Changsha, 410111, China

<sup>4</sup>Department of Precision Mechanical Engineering, Shanghai University, Shanghai, 200444, China

\*Corresponding author: Xiangliang JIN      E-mail: jinxl@xtu.edu.cn

**Abstract:** Two silicon-based ultraviolet (UV) and blue-extended photodiodes are presented, which were fabricated for light detection in the ultraviolet/blue spectral range. Stripe-shaped and octagon-ring-shaped structures were designed to verify parameters of the UV-responsivity, UV-selectivity, breakdown voltage, and response time. The ultra-shallow lateral pn junction had been successfully realized in a standard 0.5- $\mu\text{m}$  complementary metal oxide semiconductor (CMOS) process to enlarge the pn junction area, enhance the absorption of UV light, and improve the responsivity and quantum efficiency. The test results illustrated that the stripe-shaped structure has the lower breakdown voltage, higher UV-responsivity, and higher UV-selectivity. But the octagon-ring-shaped structure has the lower dark current. The response time of both structures was almost the same.

**Keywords:** Ultraviolet/blue photodiode, ultraviolet responsivity, breakdown voltage, transient response, CMOS

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## 1. Introduction

The ultraviolet detection technology is developed after the infrared and laser detection technologies, and ultraviolet (UV) detectors are hotly researched and used in many application areas, e.g., in environmental monitoring [1] or in biochemical analysis [2]. Photodiodes used for UV detecting are required to be sensitive to blue/UV radiation and blind to visible and near-infrared radiation. Different structures have been reported to realize UV silicon photodetectors. A. R. Pauchard [3] and Ayman Ghazi [4] proposed the silicon based UV photodiodes fabricated in the standard

complementary metal oxide semiconductor (CMOS) process. The first ultraviolet avalanche photodiode in the CMOS technology was presented by A. Pauchard [5], and a responsivity of about 2.3 A/W at 400 nm was achieved for a reverse bias of 19.1 V. The development of phototransistors with the high responsivity for the UV/blue spectral has attracted much interest in recent years [6, 7].

Several main and important problems should be considered in the study of the silicon-based UV photodiode in the standard CMOS process: (1) the noise and leakage current on the silicon surface [8, 9], (2) the spectral response range of the UV

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photodetector and the penetration depth of UV light into the silicon material [10, 11], (3) the fabrication of the ultra-shallow pn junction in the CMOS process [12–14], and (4) a decrease in the breakdown voltage or operation voltage of the photodiode for silicon-on-a-chip (SoC) integration [15–17]. To optimize the noise performance of the UV photodiode, the processes of doping and isolation need to be improved. However, changing or adding process steps are too expensive. In this paper, an extremely thin layer with  $p^+$  doping is injected on the crystal surface to reduce the defects, noise, and leakage current. The silicon-based UV photodiode can be fabricated with the readout circuit on a same chip when the working voltage is compatible to the CMOS process. Strip-shaped structures have been proposed to increase the absorption of UV light and reduce the breakdown voltage [3–5]. Various characteristics of the parameter were obtained for different UV photodiode structures.

In this paper, the stripe-shaped and octagon-ring-shaped silicon-based UV and blue-extended photodiodes are presented, which were fabricated to verify and compare their parameters: UV-responsivity, UV-selectivity, breakdown voltage, and response time.

## 2. Design and fabrication

### 2.1 Structure description

Figure 1 shows the top view of the two proposed structures, Fig. 1(a) presents the stripe-shaped photodiode, and Fig. 1(b) presents the octagon-ring-shaped photodiode. They are actually conventional  $p^+$ - $n_{\text{well}}$ - $p_{\text{sub}}$  structures, and the schematic cross-section of them is shown in Fig. 1(c). The highly doped  $p^+$  octagon-ring-shaped anodes are bounded by the  $n_{\text{well}}$  both laterally and vertically. The optical window of the structure is covered by an anti-reflection coating, which consists of a layer of  $\text{SiO}_2$  with a thickness of 60 nm. The silicon surface

is injected with high  $p^+$  doping and forms an extremely thin layer. The width of each anode is  $3.0\ \mu\text{m}$ ; the distance between two adjacent anodes is  $1.5\ \mu\text{m}$ . The total area of both photodiodes is about  $\pi \cdot (50 \times 50)\ \mu\text{m}^2$ . The  $p_{\text{sub}}$ - $n_{\text{well}}$  junction of this device is short-circuited in order to achieve the better UV selectivity.

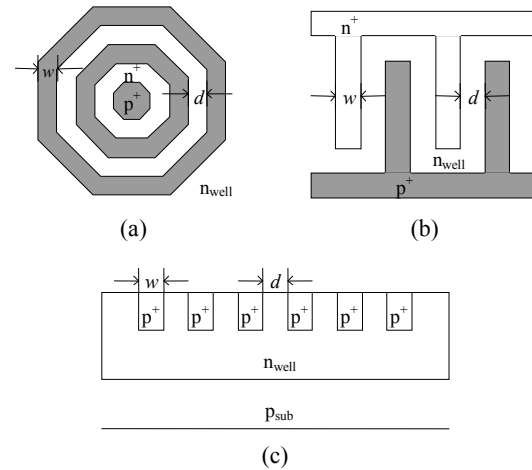


Fig. 1 Structures of the two photodiodes: (a) top view of the octagon-ring-shaped photodiode, (b) top view of the stripe-shaped photodiode, and (c) schematic cross-section of two UV photodiodes, where  $w$  is the anode width and  $d$  is the space between two anodes.

### 2.2 Device fabrication

The UV/blue-extended photodiodes were fabricated by the standard  $0.5\text{-}\mu\text{m}$  CMOS process. The microphotographs are shown in Fig. 2. Figure 2(a) is the octagon-ring-shaped photodiode (Structure 1) with four laps of  $p^+$  anodes, one  $n^+$  cathode, and one  $p^+$  substrate, and Fig. 2(b) is the stripe-shaped photodiode (Structure 2), which has eight stripes of  $p^+$  anodes, one stripe of  $n^+$  cathode and one stripe of  $p^+$  substrate. The two photodiodes have an equivalent area so as to make better comparisons. Their  $p^+$  anodes are connected through metals, respectively. Their  $n^+$  cathode and  $p^+$  substrate are short-circuited to make the photodiodes much more sensitive to UV light than to visible and near infrared radiation. Two pads are connected with the anode and cathode, respectively. The avalanche photodiode (APD) photodiode tester (GCAPD-B), oscilloscope (Tektronik MSO-2024), and micro-

ammeter (HB-321) were used to test the proposed photodiodes.

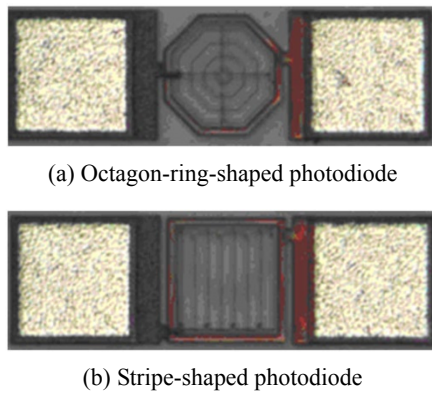


Fig. 2 Microphotographs of (a) the octagon-ring-shaped photodiode and (b) the stripe-shaped photodiode.

### 3. Silicon test results

#### 3.1 Spectral responsivity

The spectral responsivities of those two UV/blue photodiodes are shown in Fig. 3. The reverse bias voltage was set at less than 16 V, and the illumination intensity was set at 500 lx. It can be seen that in the UV/blue spectrum ( $0.3\ \mu\text{m} - 0.5\ \mu\text{m}$ ), the spectral responsivity of Structure 2 was larger than that of Structure 1. The peak photocurrent responses of the two photodiodes were about  $2.51 \times 10^{-8}\ \text{A}$  (at 420 nm) and  $2.38 \times 10^{-8}\ \text{A}$  (at 450 nm). However, the photocurrent response of Structure 2 becomes smaller than that of Structure 1 within the visible and IR range ( $0.5\ \mu\text{m} - 1\ \mu\text{m}$ ). At the wavelength of  $1\ \mu\text{m}$ , the photocurrent response of Structure 2 was  $3.4 \times 10^{-11}\ \text{A}$  while Structure 1 got  $5.41 \times 10^{-10}\ \text{A}$ . In this paper, the UV-selectivity is defined as the ratio of the photocurrent response at  $0.4\ \mu\text{m}$  and  $1\ \mu\text{m}$ . Structure 2 obtained an UV-selectivity of 560 while Structure 1 just obtained an UV-selectivity of 400. To sum up, the stripe-shaped photodiode performs better in UV-reponsivity and UV-selectivity. Structure 1 has more areas of  $p^+$  anode through calculation, which means that its dead layer [3] area is larger than that of Structure 2. The dead layer will decrease the UV-responsivity and UV-selectivity of the

photodiode as described in [3].

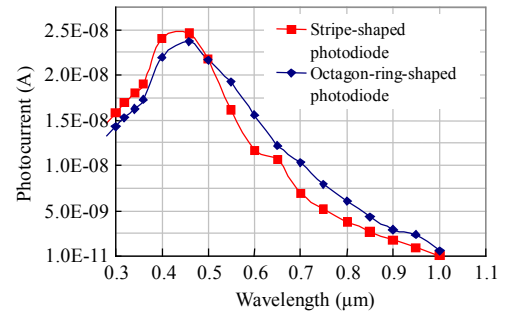


Fig. 3 Tested spectral responsivity (photocurrent response) of two UV/blue-extended photodiodes.

#### 3.2 $I$ - $V$ characteristic curves

The comparison of the  $I$ - $V$  characteristics of those two UV photodiodes are shown in Fig. 4. It is evident to see that the breakdown voltage of Structure 1 is about 22.5 V while the other one of Structure 2 is about 17.2 V. The photodiode with the stripe-shaped structure has the lower breakdown voltage than that of Structure 2. Because the rectangle mask was used to fabricate the stripe-shaped ships. The spherical pn junction was

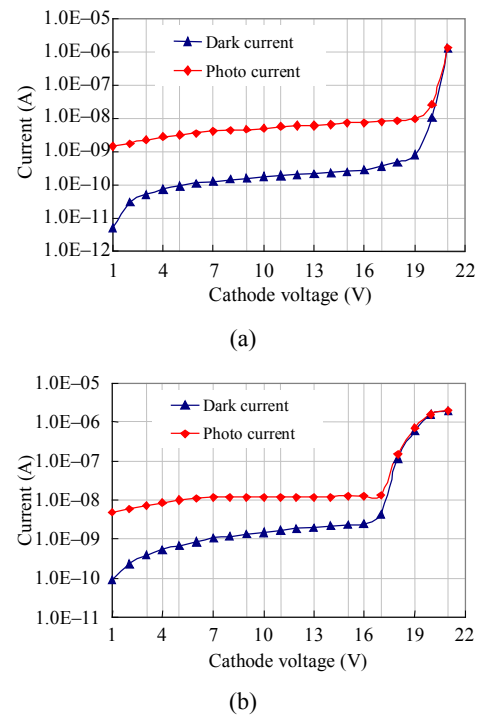


Fig. 4  $I$ - $V$  characteristics of the two photodiodes, (a)  $I$ - $V$  curves of Structure 1, breakdown voltage of which is about 20.5V, and (b)  $I$ - $V$  curves of Structure 2 whose breakdown voltage is about 17.2V.

formed in angles of 90 degrees where the electric field was highly concentrated. It is known that the spherical pn junction has the largest electric field compared to the plane pn junction and cylindrical pn junction under a condition of the same substrate material, the same doping concentration, and the same bias voltage. Avalanche breakdown occurs easily in the spherical pn junction and cylindrical pn junction especially for very shallow pn junctions, which will reduce the avalanche voltage of the photodiode. However, edge breakdown will occur easily when the photodiode is under a voltage that is higher than the avalanche voltage, which increases the edge dark current and decreases the ratio of signal to noise. As a result, early edge breakdown should be avoided. Unfortunately, the stripe-shaped photodiode performs well but has a bigger dark current.

### 3.3 Transient response

The response time reflects how fast the UV photodiode is when it is biased and illuminated. Usually, the rise time and fall time are both considered. The response time of the proposed photodiodes are shown in Fig. 5. For Structure 1, its rise time and fall time are 8 nanoseconds and 2 nanoseconds, respectively. And for Structure 2, its rise time and fall time are 5 nanoseconds and 2 nanoseconds, respectively. As there are much more spherical pn junctions in Structure 2, the transport velocity of carriers are raised, and the response time is cut down. From another point of view, the octagon-ring-shaped photodiode has the highly symmetrical structure, the total time of diffusion and drifting are longer than that of the stripe-shaped photodiode, because there are much more phenomena of carriers diffusion in the octagon-ring-shaped photodiode. Although the difference of response time of both photodiodes is not clear, it can be predicted that the stripe-shaped photodiode would get even smaller response time if bigger structures or bigger arrays of the photodiode are

fabricated.

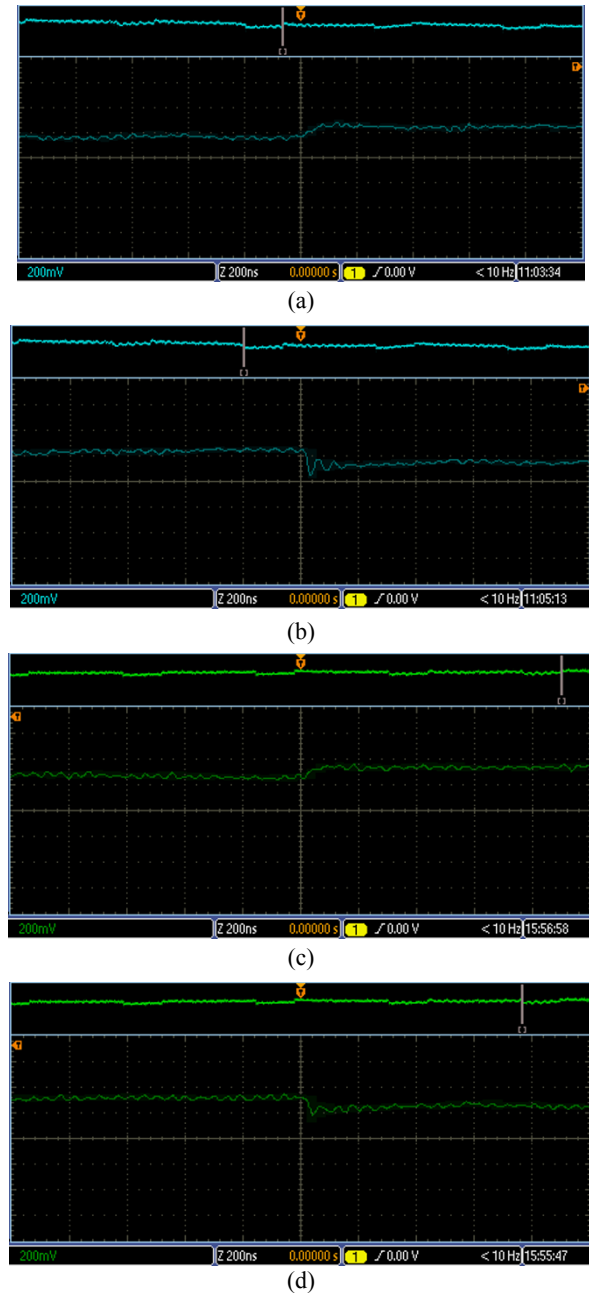


Fig. 5 Transient response of the two photodiodes: (a) rise time of Structure 1 is 8 ns, (b) fall time of Structure 1 is 2 ns, (c) rise time of Structure 2 is 5 ns, and (d) fall time of Structure 2 is 2 ns.

## 4. Conclusions

In conclusion, this paper presents and fabricated two silicon-based UV and blue-extended photodiodes. Stripe-shaped and octagon-ring-shaped structures were designed to verify and compare photodiode parameters of the UV-responsivity,

UV-selectivity, breakdown voltage, and response time. The ultra-shallow lateral pn junction has been successfully realized in a standard 0.5- $\mu\text{m}$  CMOS process to enlarge the pn junction area, enhance the absorption of UV light, and improve the responsivity and quantum efficiency. The test results illustrate that the stripe-shaped structure has the lower breakdown voltage, higher UV-responsivity, and higher UV-selectivity. But the octagon-ring-shaped structure has the lower dark current. The rise time of the stripe-shaped photodiode is small than that of the octagon-ring-shaped photodiode. Although there is not big difference in the response time of two structures, the conclusions in this paper can predict that the stripe-shaped photodiode would get even less response time if the bigger structures or bigger arrays of the photodiode are fabricated. The work in this paper is significant to help analyzing the performance of the silicon-based UV/blue photodiodes.

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